

**UNITED STATES PATENT APPLICATION**

**OF**

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**FOR**

**MULTIBAND, SINGLE ELEMENT  
WIDE FIELD OF VIEW INFRARED IMAGING SYSTEM**

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**MULTIBAND, SINGLE ELEMENT  
WIDE FIELD OF VIEW INFRARED IMAGING SYSTEM**

**BACKGROUND**

**FIELD OF INVENTION:**

[0001] The present device relates generally to an infrared imaging system. More specifically, the device relates to wide field of view, infrared imaging systems with mid-wave infrared bands and, optionally long-wave infrared bands.

**BACKGROUND INFORMATION:**

[0002] Infrared electromagnetic radiation refers to the region of the electromagnetic spectrum between wavelengths of approximately 0.7 and 1000  $\mu\text{m}$ , which is between the upper limit of the visible radiation region and the lower limit of the microwave region. Infrared radiation is sometimes broken into three sub-regions: near-infrared radiation with wavelengths between 0.7-1.5  $\mu\text{m}$ , intermediate-infrared radiation with wavelengths between 1.5-20  $\mu\text{m}$ , and far-infrared radiation with wavelengths between 20-1000  $\mu\text{m}$ . The intermediate-infrared radiation region is often further broken into the mid-wave (MWIR) region with wavelength limits of 3-5  $\mu\text{m}$  and the long-wave (LWIR) region with wavelength limits of 8-12  $\mu\text{m}$ .

[0003] Infrared radiation is produced principally by electromagnetic emissions from solid materials as a result of thermal excitation. The detection of the presence, distribution, and direction of infrared radiation requires techniques which are unique to this spectral region. The wavelengths of infrared radiation are such that optical methods may be used to collect, filter, and direct the infrared radiation. Photosensitive devices convert heat, or infrared electromagnetic radiation, into electrical energy and are often used as infrared sensitive elements.

Such photosensitive devices respond in proportion to the number of infrared photons within a certain range of wavelengths to provide electrical energy.

[0004] Generally, an imaging infrared sensor includes a plurality of infrared sensitive elements in order to provide suitable resolution of the field of view which is to be monitored. In addition to the plurality of infrared sensitive elements, an infrared sensor includes other components for complete processing of the information provided by incident infrared electromagnetic radiation. Optical filters and apertures are used to define and focus the radiation directed at the infrared sensitive elements. Electronics are necessary for controlling the data collection and processing the collected data from the infrared sensitive elements. Cooling apparatus is necessary to maintain the operation of the infrared sensitive elements as well as the electronics. One approach for processing the electrical energy provided by the plurality of infrared sensitive elements is to use multiplexers to provide a single signal having a serial data stream since it is simpler to process the single resulting serial signal than the plurality of signals which correspond to the plurality of infrared sensitive elements. The serial signal is generally further processed by any number of techniques known in the art to provide interpretable, useful information regarding objects in the field of view of the infrared sensor.

[0005] As is known in the art, military and space applications employ infrared electromagnetic radiation detection for such functions as tracking and searching. These applications require the detection of low-level radiation in the intermediate infrared radiation range. One example of an application for infrared detection is in radar systems, where greater angular resolution and obstacle penetration capabilities improve overall platform imaging capabilities while the inclusion of infrared detection, particularly the detection of more than one band, or range, of infrared radiation, makes the system more difficult to jam, or disable.

[0006] Electro-optical sensor assemblies, such as infrared imaging systems, use optical components to route and focus received radiation onto a detector.

However, the size and weight of electro-optical sensor assemblies have always been a significant design consideration. For example, in an airborne application, the size of the sensor assembly dictates the size of the required gimbal, which in turn affects the overall system size and weight. Since the sensor assembly and gimbal may both be in the airstream, the size of each can affect the overall aircraft drag. In another example, such as in ground applications, a head mirror may be used for elevation pointing. The number of optical apertures and the size of these apertures dictate the head mirror size, which, in turn, affects the size and weight of the surrounding armor plate.

#### SUMMARY

[0007] The present invention is generally directed to an infrared imaging system. The infrared imaging apparatus with a dewar has an internal volume defining a cold space. An IR transmissive window seals the cold space and receives IR energy directly from an IR source. Within the cold space, an optical stop located in front of a first lens, a first lens with aspherical surface profiles on both the first and the second surface, and an IR detector are positioned and aligned in operational communication to receive IR energy directly from the IR transmissive window and direct the IR energy to the detector coincidentally positioned at the focal plane of at least a first and second wavelength of IR energy.

[0008] The second aspherical surface profile has a holographic optical element that color corrects at least one color band of infrared energy. The holographic optical element may detect a second or subsequent wavelength of IR energy that is a harmonic component of the first wavelength. Preferably, the holographic optical element color corrects a red MWIR band and a blue MWIR band. The holographic optical element also coincidentally focuses a MWIR band and a LWIR

band of IR energy at a common focal plane. The detector detects and manipulates at least three wavelengths of IR energy including at least one LWIR band of energy, preferably an indigo LWIR band.

[0009] An exemplary infrared imaging apparatus has lens made from germanium or silicon and performs at an F-stop (F/#) of at least 1.4 with a square field of view of 90x90 degrees.

#### BRIEF DESCRIPTION OF THE DRAWING FIGURES

[0010] Objects and advantages of the invention will become apparent from the following detailed description of preferred embodiments in connection with the accompanying drawings, in which like numerals designate like elements and in which:

[0011] Figure 1 is a perspective view of the imaging system; and

[0012] Figure 2 is a schematic representation of the line trace of energy in a first embodiment of optical components.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0013] Figure 1 is a perspective view of an infrared imaging system **100**. The infrared imaging system **100** has a compressor housing **102** and an optical housing **104**. The optical housing **104** further has a cryogenic subassembly **106**, an optical subassembly **108**, and an electronics subassembly **110**.

[0014] The compressor housing **102** contains suitable support components required to maintain cooling of the optical housing **104**. Specifically, the compressor housing **102** can contain a compressor for circulating a cooling medium through the compression and expansion cycle used for cooling.

[0015] The cryogenic subassembly **106** has a cavity **114**, alternatively called a dewar, which defines a cold space **116**. Infrared energy detectors generally require cooling to improve performance in converting incident energy into an electrical signal. The cryogenic subassembly **106** provides the required cryogenic

cooling capability. The cavity **114** is in fluid communication with the compressor housing **102** through the transfer line **112**. The cooling medium, such as liquid nitrogen (LN2), is circulated in a closed loop from the compressor, through the transfer line **112**, and through the cavity **114**. The cold space **116** is sealed by an IR transmissive window **120** and is evacuated to < 50 mTorr, preferably less than 5 mTorr.

[0016] The optical subassembly **108** is positioned within the cold space **116** at the receiving end **118** of the optical housing **104**. Elements of the optical subassembly **108**, including a lens **122** and an IR detector **124**, are housed in the cold space **116**. Elements of the optical subassembly **108** are maintained at a suitable cryogenic temperature by the cryogenic subassembly **106**, typically 150 to 180° K.

[0017] The electronics subassembly **110** receives inputs from the IR detector **124** and transmits signals to a processing unit (not shown).

[0018] Figure 2 shows a plan cross-section of a first embodiment of an optical subassembly **200**. The optical subassembly **200** has an IR transmissive window **202**, an optical stop **204**, a lens **206**, and an IR detector **208**. The optical stop **204**, lens **206**, and IR detector **208** are positioned inside the cold space **210** of the cryogenic subassembly **106** shown in Figure 1. An example of an IR transmissive window **202** is optical grade germanium or an amorphous solid, such as zinc selenide. The IR transmissive window **202** has a 120° circular field of view and receives incident IR energy directly from an IR source. In an alternative embodiment, there may be an additional filter placed before the IR transmissive window **202** that discriminates a desired wavelength of energy or wavelengths of energy.

[0019] The optical stop **204** is positioned in the cold space **210** at the limiting aperture in the transmission path where the incident energy has a first crossover

point **A**. The position of the optical stop **204** may be abutting the lens **206** or it may abut the IR transmissive window **202** and will be determined by the wavelengths of energy to be detected and the characteristics of the other optical components. In a preferred embodiment, the optical stop **204** may be from 20/1000th to 60/1000th from the lens **206**; more preferably the optical stop **204** is 40/1000th from the lens **206**. The optical stop **204** has an opening **212** circularly symmetric about axis X-X', the radius of which is the size of the cross-section of the caustic at the first crossover point **A**. The caustic is the envelope curve of the transmitted beam. The optical stop **204** helps to prevent stray energy from traveling down the transmission path toward the lens **206** and thus improves optical performance. By placing the optical stop **204** within the cold space **210** and in front of the lens **206**, design requirements are simplified while still maintaining the required cold shield efficiency.

[0020] A first surface **214** of the lens **206** is oriented toward the IR transmissive window **202** and a second surface **216** that is oriented toward the detector **208**. IR energy **218** is directly received by the lens **206** from the IR transmissive window **202**. The first and second surfaces **214**, **216** of the lens **206** are aspherical over at least a portion of the lens **206** and such that the aspherical surfaces **220** are aligned radially symmetric in the transmission path about axis X-X'. Alternatively, the entire first or second surface **214**, **216** may be aspherical. However, the cross-section of the caustic at the points **B**, **C** is no greater than the surface area of the first or second surface **214**, **216** and is such that the transmission path may propagate through the aspherical surfaces **220**.

[0021] The second surface **216** of the lens **206** is also a holographic optical element (HOE) **222**, alternatively called a binary surface or a diffractive grating on a curved surface. The HOE **222** uses principles of harmonics to discriminate and propagate a plurality of wavelengths. Preferably, the HOE **222** discriminates and

propagates at least two wavelengths. For example, a first wavelength is manipulated by the HOE **222**, a second wavelength must be a harmonic component of the first wavelength for the HOE **222** to manipulate it. The requirement applies to all subsequent wavelengths to be manipulated by the HOE **222**.

[0022] A detector **208** is positioned in alignment with the other components of the optical subassembly **200** about the axis X-X' at a focal length distance **d** from the second surface **216** of the lens **206**, at a coincident focal plane to at least 2 wavelengths manipulated and transmitted by the lens **206** and the HOE **222**. The detector **222** can discriminate at least two, and preferably multiple, wavelengths of incident energy in the IR spectrum, and more preferably wavelengths at 3-12  $\mu\text{m}$ . The detector **208** processes the wavelengths to produce multiple waveband detection capability within a single detector. In one embodiment, the detector **208** concurrently collects radiation from multiple, adjacent spectral radiation bands. This type of detector may be used in "hyperspectral imaging." An example of such a detector is disclosed in co-assigned U.S. Patent No. 6,180,990 B1, issued to Claiborne et al., the disclosure of which is incorporated herein by reference.

[0023] In an another embodiment, the detector **208** may manipulate multiple wavelengths of incident energy resulting in at least two MWIR and one LWIR band being detected by the infrared imaging system **100**. A detector capable of hyperspectral imaging is suitable for this application.

[0024] The first and second aspherical surfaces **214,216** and the HOE **222** combine to manipulate infrared energy from at least two wavebands in the infrared spectrum. In one embodiment, a first waveband is a mid-wave infrared (MWIR) waveband with wavelength of 3-5  $\mu\text{m}$ , preferably 4-4.5  $\mu\text{m}$ , and a second waveband is a mid-wave infrared (MWIR) waveband with wavelength of 3-5  $\mu\text{m}$ , preferably 4-4.5  $\mu\text{m}$ . In a second embodiment, the first and second aspherical surfaces **214,216**, the HOE **222**, and the detector **208** combine to manipulate

infrared energy from at least two wavebands in the infrared spectrum. In this embodiment, a first and second waveband similar to the first embodiment is detected. A detector **208**, as described above, can be a detector suitable for hyperspectral imaging and can manipulate and discriminate a third coincident and coregistered waveband. This third waveband may be a LWIR waveband with wavelength of 8-12  $\mu\text{m}$ , preferably 8.5-9.5  $\mu\text{m}$ .

[0025] An aspherical surface may be mathematically defined by:

$$H(x) = \frac{rx^2}{1 + \sqrt{1 - r^2(k+1)x^2}} + ax^4 + bx^6 + cx^8 + dx^{10} \quad \text{Eq. 1}$$

where  $r$  = radius of curvature,  $k$ =conic coefficient, and  $a$ ,  $b$ ,  $c$ , and  $d$  are aspheric coefficients.

[0026] There is a correspondence between the conic coefficient of Eq. 1 and the geometric surface profile. Table 1 illustrates this correspondence.

Table 1: Correspondence between  $k$  and the type of profile

| Value of $k$ | Type of Profile |
|--------------|-----------------|
| $>0$         | ellipse         |
| $=0$         | sphere          |
| $-1 < k < 0$ | ellipse         |
| $=-1$        | parabola        |
| $<-1$        | hyperbola       |

[0027] In practice, one skilled in the art could utilize commercially available lens design software to obtain suitable values for the coefficients of Eq. 1, including the aspherical coefficients. An example of one such lens design software

package is "CODE V®" available from Optical Research Associates of Pasadena, California. One skilled in the art could input information including, for example, image size, focal distance, energy distribution across the detector and determine the optimized values for the coefficients of Equation 1. Examples of suitable coefficients for use in an infrared imaging detector in keeping with this invention are shown in Table 2 and 3.

[0028] Table 2 is a first embodiment of an optical prescription for the lens **206** of the single element wide field of view infrared imaging system **100**. This example is a prescription for a dual band lens.

Table 2. Prescription of Dual Band Lens

| #                         | Description    | Radius   | k          | Thickness | a        | b        | c       | d        |
|---------------------------|----------------|----------|------------|-----------|----------|----------|---------|----------|
| 1                         | First Surface  | -0.94467 | 28.345216  | 0.548467  | -2.13952 | -69.5274 | 2342.04 | -56841.9 |
| 2                         | Second Surface | -0.61281 | 0.1399     | 0.462731  | 0.033459 | -2.3598  | 10.889  | -36.331  |
| HOE Coefficients (Radial) |                |          | -0.0051393 | -0.10212  | 0.91035  | -2.3946  |         |          |
| 3                         | Focal Plane    |          |            |           |          |          |         |          |

[0029] Table 3 is a second embodiment of an optical prescription for the lens **206** of the single element wide field of view infrared imaging system **100**. This example is a prescription for a three band lens.

Table 3. Prescription of Three Band Lens

| #                        | Description    | Radius   | k         | Thickness | a        | b        | c       | d       |
|--------------------------|----------------|----------|-----------|-----------|----------|----------|---------|---------|
| 1                        | First Surface  | -1.23508 | 36.049455 | 0.761661  | -1.69104 | -98.6413 | 5589.83 | -162359 |
| 2                        | Second Surface | -0.81270 | -0.10748  | 0.480234  | 0.054475 | -0.72423 | 2.9155  | -7.8939 |
| HOE Coefficients(Radial) |                |          | -0.017112 | -0.038991 | 0.55069  | -1.6405  |         |         |
| 3                        | Focal Plane    |          |           |           |          |          |         |         |

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[0030] In Tables 2 and 3, "Radius" is the radius of curvature ( $r$ ),  $k$  is the conic coefficient, and  $a$ ,  $b$ ,  $c$ , and  $d$  are the aspherical coefficients. The "thickness of the first surface" is the thickness of the lens **206**. The "thickness of the second surface" is the back focal distance, which is the distance from the second surface **216** of the lens **206** to the detector **208**, or focal distance  $d$ .

[0031] The optical performance of an infrared imaging system **100** in keeping with the embodiments described may have an optical  $F/\# = 1.4$  with a square field of review of  $90 \times 90$  degrees. Additionally, the infrared imaging system **100** has a wide field of view (field of view greater than  $60^\circ$ ).

[0032] In operation, incident infrared energy **218** travels through the limiting aperture of the optical stop **204** and is incident to the aspherical portion **220** of the first surface **214** of the lens **206**. The infrared energy **218** then is translated by the aspherical surface of the second surface **216** of the lens **206** and the HOE **222** and is focused onto the detector **208**.

[0033] In an embodiment of an optical layout in keeping with the invention, the incident infrared energy is color corrected to realize at least one band of energy on the detector surface. For example, in the first embodiment the incident infrared energy is color corrected across both the red and blue MWIR bands. In the alternative optical layout, the incident infrared energy is color corrected across the red MWIR, blue MWIR, and indigo LWIR bands.

[0034] The single lens **206** is made of silicon and has aspheric surface profiles on both sides. Alternatively, the single lens **206** may be made of germanium. The HOE **222** helps to achieve the required color correction across both the red and blue MWIR bands. The color correction across the indigo LWIR bands is provided by the detector **208** in conjunction with the HOE **222**. The optic performs at an  $F/\#$  of 1.4 with a square field of view of  $90$  by  $90$  degrees.

[0035] The use of a single, color corrected element in the dewar provides an optical subassembly **200** that is shorter and provides for a better form factor and lower part count for the entire infrared imaging system **100**. Also, by enclosing the single lens **206** within the detector dewar, the optical subassembly **200**, including the optical stop **204**, lens **206** and detector **208**, are all located within a single enclosure. Previously, tight alignment tolerances had to be maintained across the detector-to-dewar mount, the dewar-to-optical housing mount and the optical housing-to-optics mount. By eliminating the multiple interfaces the total tolerance budget can be applied on the single interface, reducing the required manufacturing and assembly tolerances and reducing the requirement for precision alignment across multiple interfaces.

[0036] Another advantage of being able to place the single, color corrected lens **206** in the cryogenic subassembly **106** is that it places the optical subassembly **200** in a controlled temperature environment. By maintaining the lens **206** at a nearly constant temperature, the need for a passive or active athermalization system to correct the thermally induced focus variations may be eliminated. While this could be accomplished previously by heating or cooling the optics with a separate device, this approach makes use of the cooling capabilities that are already present in the system.

[0037] The alignment of the optical components is important so that a detector is located at the focal plane for the lens system. In previous multi-lens imaging systems, it was difficult to ensure alignment of the optical components because the thermal coefficient of expansion resulted in disparate movement of the individual optical components. A unitary structure housed within the cold space essentially eliminates thermal transients amongst the components once a temperature equilibrium has been achieved by the cryogenic housing and compressor, thereby overcoming the alignment problems.

[0038] Also, enclosing the optical subassembly **200** in the cryogenic subassembly **106** places the optics in a sealed, evacuated environment, protecting it against dust or other contamination. While this could be accomplished in a separate enclosure, this approach makes use of capabilities already present in the optical housing **104**.

[0039] Lastly, all of these qualities permit the design of a lower cost system with the same performance capabilities of current, more expensive ones.

[0040] In one exemplary application, the use of wide field of view (greater than 100°) MWIR imaging systems on military platforms provides the capability of performing missile warning, defensive infrared search and track, navigation and situational awareness functions. Adding a second wave band to the sensor helps to discriminate between natural and manmade objects and increases the effectiveness of the sensor in these tasks. Additionally, adding a third LWIR band to the sensor further improves the imaging system's ability to discriminate between natural and manmade objects and increases the effectiveness of the sensor in these tasks. Since providing complete spherical coverage around an object requires a maximum of six sensors, the cost, size and complexity of current systems can prohibit their large scale employment.

[0041] This invention has direct application to other wide field of view multiband uses, including but not limited to dual band navigation, advanced missile seekers and chemical agent detection.

[0042] Although the present invention has been described in connection with preferred embodiments thereof, it will be appreciated by those skilled in the art that additions, deletions, modifications, and substitutions not specifically described may be made without department from the spirit and scope of the invention as defined in the appended claims.